

DIELECTRIC FILTER, ANTENNA SHARING DEVICE, AND  
COMMUNICATION DEVICE

BACKGROUND OF THE INVENTION

5    1.   Field of the Invention

The present invention relates to a dielectric filter for use in a microwave band, an antenna sharing device, and a communication device.

2.   Description of the Related Art

10       Conventionally, band-pass filters and band-block filters have been known, in which a reactance element such as a PIN diode or variable capacitance diode is connected to a coaxial dielectric resonator, whereby the resonance frequency of each filter can be shifted  
15 by voltage control of the reactance element.

FIG. 18 is a plan view showing the configuration of a conventional variable frequency band-pass filter 1. FIG. 19 is an electric circuit diagram of the band-pass filter. The filter 1 comprises resonance  
20 circuits coupled in two stages, and comprises dielectric resonators 2 and 3, coupling capacitors C5, C6 and C7, polarization capacitors C1 and C2 for producing an attenuation pole, frequency shifting capacitors C3 and C4, PIN diodes D1 and D2 as  
25 reactance elements, inductors L1 and L2 to function as choke coils, control voltage supply resistors R1 and R2, capacitors C8 and C9, and a circuit substrate 5 (Fig. 18) for mounting these parts. Moreover, an

input terminal electrode P1, an output terminal electrode P2, voltage control terminal electrodes CONT1 and CONT2, and ground patterns G1 and G2 are shown.

5           Although the circuit of Figs. 18-19 functions well, the number of parts contained in the conventional variable frequency band-pass filter 1 is large, so that miniaturization of the circuit has been difficult. A particular problem is that the space  
10           occupied by the circuit elements such as the PIN diodes or the like on the circuit substrate 5 is substantially equal to the space occupied by the dielectric resonators 2 and 3.

          Moreover, conventionally, when a greater range of  
15           frequency shift is desired, the electrostatic capacitances of the frequency shifting capacitors C3 and C4 are increased. However, the interaction between the frequency shifting capacitors C3 and C4 and the PIN diodes D1 and D2 presents a problem. When  
20           the PIN diodes D1 and D2 are on, the frequency shifting capacitors C3 and C4 are dominant, respectively, as the capacitance components of the resonance circuits of the variable frequency band-pass filter 1 shown in FIG. 19. When the PIN diodes D1 and  
25           D2 are off, the capacitance between the anode and cathode terminals of each of the diodes D1 and D2

becomes dominant. For this reason, if the capacitances of the frequency shifting capacitors C3 and C4 are increased, there will be a large difference between the impedance of the resonance circuit when the PIN diodes D1 and D2 are on, and that obtained when the diodes D1 and D2 are off. Therefore, the pass-band width obtained when the PIN diodes D1 and D2 are on (that is, when the pass frequency of the filter 1 is low) is narrower than that obtained when the diodes D1 and D2 are off (that is, when the pass frequency of the filter 1 is high). Accordingly, the available range of frequency shift has a limitation. The design flexibility is low.

#### 15 SUMMARY OF THE INVENTION

Responding to these concerns, the present invention provides a dielectric filter which has great flexibility regarding the available frequency shift range, has a small number of parts, and is small in size.

The invention also provides an antenna sharing device and a communication device using the filter.

To provide these features, according to the present invention, there is provided a dielectric filter which comprises a dielectric block having at least one resonance electrode, input and output

terminal electrodes to be connected to external circuits, and a separated electrode provided on the outer face of the dielectric block, not connected to the input and output terminals and ground, and  
5 connected to the resonance electrode via a capacitance. The separated electrode and the input and output terminal electrodes are provided on the outer face of the dielectric block or optionally on the surface of a circuit substrate.

10 With the above-described configuration, the resonance electrode provided on the dielectric block constitutes a resonator. On the other hand, the separated electrode generates capacitance between the separated electrode and the resonance electrode, which  
15 functions equivalently to a frequency shifting capacitor. Accordingly, it is unnecessary to provide a separate frequency shifting capacitor.

Preferably, a voltage controllable reactance element and a circuit element for controlling the  
20 reactance element are electrically connected to the separated electrode. Thereby, the reactance element is voltage-controlled to be switched, so that the frequency shifting capacitor, formed by the separated electrode, is grounded or opened to change the  
25 frequency characteristic of the filter. Here, the dielectric block, the reactance element, and the

circuit element may be mounted onto the circuit substrate so that the reactance element and the circuit element are electrically connected to the separated electrode via a circuit pattern provided on the circuit substrate. As the voltage controllable reactance element, for example, a PIN diode, field effect transistor, or a variable capacitance diode may be used.

Furthermore, by electrically connecting at least two separated electrodes via the coupling adjustment element, the filter band-widths obtained when the voltage controllable reactance element is on and that obtained when the element is off can be independently set. As the coupling adjustment element, for example, a reactance element such as a capacitor, an inductor, or the like, and a variable capacitance capacitor, and so forth may be employed.

Moreover, according to the present invention, there is provided a dielectric filter which comprises a dielectric block having at least one resonance hole, a conductor inserted into the resonance hole while the conductor is insulated from an inner conductor of the resonance hole, a voltage-controllable reactance element electrically connected to the conductor, and a circuit substrate for the reactance element to be mounted onto, disposed on an outer face of the

dielectric block excluding the under face thereof.  
Thereby, the inner conductor of the resonance hole and  
the conductor inserted into the resonance hole form a  
frequency shifting capacitor. Thus, it is unnecessary  
5 to provide a conventional frequency shifting capacitor  
element.

Moreover, according to the present invention,  
there is provided a dielectric filter comprising a  
dielectric block having at least one resonance hole, a  
10 conductor electrically connected to an inner conductor  
of the resonance hole, a voltage-controllable  
reactance element electrically connected to the  
conductor, and a circuit substrate for the reactance  
element to be mounted onto, disposed on an outer face  
15 of the dielectric block excluding the under face  
thereof. Onto the circuit substrate, a circuit  
element for controlling the frequency shifting  
capacitor element and the reactance element, and so  
forth may be mounted in addition to the reactance  
20 elements.

Preferably, either a step or a concavity is  
provided on the dielectric block, and the separated  
electrode is provided on the step or in the concavity.  
Thus, since the reactance element and the circuit  
25 element are mounted on the step or in the concavity,  
the dielectric filter is reduced in size.

The antenna sharing device and the communication device of the present invention each include at least one of the dielectric filters having the above-described characteristics. Therefore, the design flexibility can be enhanced, and the size can be reduced.

Other features and advantages of the present invention will become apparent from the following description of the invention which refers to the accompanying drawings, in which like references denote like elements and parts.

#### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is an exploded perspective view of a dielectric filter according to a first embodiment of the present invention;

FIG. 2 is an electrically equivalent circuit diagram of the dielectric filter of FIG. 1;

FIG. 3 is an electric circuit diagram illustrating the operation of the dielectric filter, when a PIN diode is on.

FIG. 4 is an electric circuit diagram illustrating the operation of the filter when the PIN diode is off.

FIG. 5 is an exploded perspective view of a dielectric filter according to a second embodiment of

the present invention;

FIG. 6 is an exploded perspective view of a dielectric filter according to a third embodiment of the present invention;

5        FIG. 7 is an exploded perspective view of a dielectric filter according to a fourth embodiment of the present invention;

FIG. 8 is an exploded perspective view of a dielectric filter according to a fifth embodiment of  
10 the present invention;

FIG. 9 is an exploded perspective view of a dielectric filter according to a sixth embodiment of the present invention;

FIG. 10 is an exploded perspective view of a  
15 dielectric filter according to a seventh embodiment of the present invention;

FIG. 11 is an exploded perspective view of a dielectric filter according to a eighth embodiment of the present invention;

20        FIG. 12 is an exploded perspective view of a dielectric filter according to a ninth embodiment of the present invention;

FIG. 13 is a cross sectional view taken along line XIII-XIII before the PIN diodes are mounted as  
25 shown in FIG. 12;

FIG. 14 is a cross sectional view taken along



line XIV-XIV before the PIN diodes are mounted as shown in FIG. 12;

FIG. 15 is an exploded perspective view of a dielectric filter according to a tenth embodiment;

5        FIG. 16 is an electric circuit block diagram of an antenna sharing device according to an embodiment of the present invention;

FIG. 17 is an electric circuit block diagram of a communication device according to an embodiment of the  
10 present invention;

FIG. 18 is a plan view of a conventional dielectric filter; and

FIG. 19 is an electric circuit diagram of the dielectric filter of FIG. 18.

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#### DESCRIPTION OF EMBODIMENTS OF THE INVENTION

Hereinafter, embodiments of the dielectric filter, the antenna sharing device, and the communication device of the present invention will be  
20 described with reference to the accompanying drawings. In the respective embodiments, similar components and similar parts are designated by the same reference numerals, and the repeated description is omitted.

#### (First Embodiment, FIGS. 1 to 4)

25        A variable frequency band-pass dielectric filter 11 contains a single dielectric block 12 having a

substantially rectangular parallelepiped shape, as shown in FIG. 1. In the dielectric block 12, two resonance holes 13 and 14 are formed so as to pass through the opposing end faces 12a and 12b of the block 12. The resonance holes 13 and 14 are arranged so that the axes thereof are in parallel to each other in the dielectric block 12. The resonance holes 13 and 14 each have a circular cross section. Inner conductors 16 are formed on the inner walls of the resonance holes 13 and 14. The resonance holes 13 and 14 and the inner conductors 16 form resonance electrodes, respectively. The resonance holes 13 and 14 are coupled by electromagnetic fields to each other.

15        A step 18 is formed on the upper face 12c of the dielectric block 12 so as to form a lower portion 19. Separated electrodes 24 and 25 are formed on the lower portion 19. Chip parts (described later) such as the PIN diodes D11 and D12, and so forth are also mounted on the lower portion 19. Accordingly, because the chip parts are mounted onto the lower portion 19 of the upper face 12c of the dielectric block 12, the overall height of the filter 11 can be reduced and made small. Needless to say, it is not necessary to form the step 18 on the upper face 12c of the dielectric block 12.

On the outer face of the dielectric block 12, an outer conductor 17, an input terminal electrode 21, an output terminal electrode 22, a voltage control terminal electrode 23, and the two separated  
5 electrodes 24 and 25 are formed. The outer conductor 17 is formed on the outer face of the dielectric block 12 excluding the area where the electrodes 21 to 25 are formed and also excluding one opening end face 12a (hereinafter, referred to as an opening end face 12a)  
10 of the dielectric block 12 at which the resonance holes 13 and 14 are opened.

The input and output terminal electrodes 21 and 22 are formed so as to extend from the right and left side-faces 12d and 12e of the dielectric block 12,  
15 respectively, and then to bend and extend onto the under face 12f. The voltage control terminal electrode 23 extends from the upper face 12c of the dielectric block 12 onto the under face 12f via the side face 12e. The under face 12f is used as a  
20 mounting face of the dielectric filter 11. The dielectric filter 11 is mounted onto a printed board or the like with the under face 12f being positioned downward. The separated electrodes 24 and 25 are  
25 12 so as not to be connected to the outer conductor 17 and the other electrodes 21 to 23.

The inner conductors 16 of the resonance holes 13 and 14 are electrically opened (separated) from the outer conductor 17 at the opening side end face 12a, and are electrically short-circuited to the outer conductor 17 at the other opening end face 12b (hereinafter, referred to as a short-circuited end face 12b). Accordingly, in the dielectric block 12, the resonance holes 13 and 14 and the inner conductors 16 form  $\frac{1}{4}$  wavelength dielectric resonators R1 and R2, respectively.

Moreover, PIN diodes D11 and D12 as the voltage controllable reactance elements, and inductors L11 and L12 for voltage-controlling the PIN diodes D11 and D12, and a coupling adjustment capacitor C11, are mounted onto the upper face 12c of the dielectric block 12. The PIN diode D11 is electrically connected between the outer conductor 17 and the separated electrode 24 by means of solder or a conductive adhesive. The PIN diode D12 is electrically connected between the outer conductor 17 and the separated electrode 25. The inductor L11 and the coupling adjustment capacitor C11 are connected in parallel to each other between the separated electrodes 24 and 25. The inductor L12 is electrically connected between the separated electrode 25 and the voltage control terminal electrode 23.

For the purpose of facilitating soldering work for the respective components, a solder resist film may be printed on the lower portion 19 of the upper face 12c. Moreover, the opening end face 12a of the dielectric block 12 may be covered with a metallic sheet or the like for enhancement of the electromagnetic shielding of the dielectric filter 11.

FIG. 2 shows an electrically equivalent circuit diagram of the dielectric filter 11 constituted as described above. The dielectric filter 11 includes resonance circuits coupled in two stages. The dielectric resonator R1 is electrically connected to the input terminal electrode 21 via a coupling capacitor C13. The dielectric resonator R2 is electrically connected to the output terminal electrode 22 via a coupling capacitor C14.

The coupling capacitor C13 is formed, due to the generation of electrostatic capacitance between the input terminal electrode 21 and the inner conductor 16 of the resonance hole 13. The coupling capacitor C14 is formed, due to the generation of electrostatic capacitance between the output terminal electrode 22 and the inner conductors 16 of the resonance hole 14. The dielectric resonators R1 and R2 are electromagnetic field coupled (indicated by reference character K in FIG. 2), caused by the inner conductors

16 of the resonance holes 13 and 14 opposed to each other at an predetermined interval. Furthermore, electrostatic capacitances are generated between the input and output terminal electrodes 21 and 22 and the  
5 outer conductor 17, and thereby, capacitors C12 and C15 are formed with one end of each being grounded, respectively.

A frequency shifting capacitor Cs1 is formed, due to generation of an electrostatic capacitance between  
10 the separated electrode 24 and the inner conductor 16 of the resonance hole 13. Similarly, a frequency shifting capacitor Cs2 is formed, due to generation of an electrostatic capacitance between the separated electrode 25 and the inner conductor 16 of the  
15 resonance hole 14. That is, one end of the frequency shifting capacitor Cs1 is electrically connected to the open end of the dielectric resonator R1 via the capacitance, and the other end is electrically connected to the anode of the PIN diode D11.  
20 Similarly, one end of the frequency shifting capacitor Cs2 is electrically connected to the open end of the dielectric resonator R2 via the capacitance, and the other end is electrically connected to the anode of the PIN diode D12. The cathodes of the PIN diodes D11  
25 and D12 are grounded, respectively.

The parallel circuit of the inductor (choke coil)

L11 and the coupling adjustment capacitor C11 is connected between an intermediate connection point of the anode of the PIN diode D11 and the frequency shifting capacitor Cs1, and that of the anode of the PIN diode D12 and the frequency shifting capacitor Cs2.

The voltage control terminal electrode 23 is electrically connected to the anode of the PIN diode D12 via the choke coil inductor L12, and moreover, is electrically connected to the anode of the PIN diode D11 via the inductors L11 and L12.

As described above, in the dielectric filter 11, the frequency shifting capacitors Cs1 and Cs2 are formed by the separated electrodes 24 and 25 provided on the upper face of the dielectric block 12, and the inner conductors 16 of the resonance holes 13 and 14, respectively. Moreover, coupling between the dielectric resonators R1 and R2 is performed by utilizing the electromagnetic coupling K between the inner conductors 16 of the resonance holes 13 and 14. That is, the conventional frequency shifting capacitors and the conventional coupling capacitor between the resonators (equivalent to the coupling capacitor C6 in FIG. 18), which are separate parts from the dielectric resonators, can be omitted.

Moreover, the chip parts such as the PIN diodes

D11 and D12 or the like are mounted directly onto the dielectric block 12. Accordingly, the area occupied by the printed circuit substrate or the like of a communication device can be reduced by an amount  
5 corresponding to the direct coupling of the chip parts. Furthermore, the filter 11 having a desired attenuation pole can be obtained by appropriately designing the shapes of the resonance electrodes or those of the dielectric block, e.g., by forming large  
10 and small size portions in the resonance holes to produce a step structure. Accordingly, it is also unnecessary to provide a conventional polarization capacitor. Thus, the filter can be even more reduced in size.

15       Next, the working effects of the dielectric filter 11 will be described.

      The pass frequency of the dielectric filter 11 is determined by the resonance frequency of a resonance system comprising the frequency shifting capacitor Cs1  
20 and the dielectric resonator R1 and that of a resonance system comprising the frequency shifting capacitor Cs2 and the dielectric resonator R2. That is, when a positive control voltage is applied to the voltage control terminal electrode 23, the PIN diodes  
25 D11 and D12 are turned on. Accordingly, as shown in FIG. 3, the frequency shifting capacitors Cs1 and Cs2



are grounded via the PIN diodes D11 and D12,  
respectively, so that the pass frequency is decreased.  
At this time, the coupling adjustment capacitor C11  
exerts no influence, since it is grounded. The  
5 dielectric resonators R1 and R2 are coupled to each  
other via electromagnetic coupling K. Thus, the pass  
bandwidth of the dielectric filter 11 is set.

To the contrary, when a negative voltage is  
applied as a control voltage to the voltage control  
10 terminal electrode 23, the PIN diodes D11 and D12 are  
turned off. Thereby, as shown in Fig. 4, the  
frequency shifting capacitors Cs1 and Cs2 become open,  
and the pass frequency is increased. Then, the  
dielectric resonators R1 and R2 are coupled to each  
15 other via the electromagnetic field coupling K and the  
capacitive coupling caused by the frequency shifting  
capacitors Cs1 and Cs2, and the coupling adjustment  
capacitor C11. Accordingly, the pass bandwidth  
obtained when the PIN diodes D11 and D12 are off and  
20 that obtained when the PIN diodes D11 and D12 are on  
can be set independently with a reduced number of  
parts and a small current consumption.

As described above, the dielectric filter 11 has  
two different pass frequency characteristics, and  
25 moreover, the respective pass bandwidths can be  
independently set. In the first embodiment, the

capacitor C11 is used for adjustment of coupling between the dielectric resonators R1 and R2. However, an inductor or a voltage controllable reactance element such as a variable capacitance capacitor or  
5 the like may be used, if necessary.

(Second Embodiment, FIG. 5)

In a variable frequency dielectric filter 31, the outer conductor 17, the input terminal electrode 21, the output terminal electrode 22, and the two  
10 separated electrodes 34 and 35 are formed as shown in FIG. 5. The voltage-control terminal is not shown in Fig. 5 but can be provided as taught according to the other embodiments.

The separated electrodes 34 and 35 are formed on  
15 the opening end-face 12a of the dielectric block 12 so as not to be electrically connected to the outer conductor 17 and the input and output terminal electrodes 21 and 22. The separated electrode 35 is extended from the opening end-face 12a onto the under  
20 face 12f. A part of each of the respective separated electrodes 34 and 35 is extended into the corresponding one of the resonance holes 13 and 14. The inner conductors 16 of the resonance holes 13 and 14 serve as the resonance electrodes are opposed to  
25 the separated electrodes 34 and 35 which extend into the resonance holes 13 and 14 so as to define

conductor-free gaps 32, in the vicinity of the opening end-face 12a, respectively.

Moreover, the PIN diodes D11 and D12 and the coupling adjustment capacitor C11 are mounted on the opening end-face 12a of the dielectric block 12. The PIN diode D11 is electrically connected between the outer conductor 17 and the separated electrode 34. The PIN diode D12 is electrically connected between the outer conductor 17 and the separated electrode 35. The coupling adjustment capacitor C11 is electrically connected between the separated electrodes 34 and 35.

In the dielectric filter 31 having the above-described configuration, the frequency shifting capacitor Cs1 is formed by the separated electrode 34 and the inner conductor 16 of the resonance hole 13 which opposes each other so as to sandwich the gap 32 and generate capacitive coupling between the separated electrode 34 and the inner conductor 16. Similarly, the frequency shifting capacitor Cs2 is formed by the separated electrode 35 and the inner conductor 16 of the resonance hole 14 which oppose each other so as to sandwich the conductor gap 32 and generate electrostatic capacitive coupling between the separated electrode 35 and the inner conductor 16. As a result, the dielectric filter 31 can be reduced in size. As compared with the filter 11 of the above-

described first embodiment, the height of the dielectric filter 31 can even be more reduced.

(Third Embodiment, FIG. 6)

As shown in FIG. 6, in a variable frequency  
5 dielectric filter 41, the outer electrode 17, the input terminal electrode 21, the output terminal electrode 22, the voltage control terminal electrode 23, and two separated electrodes 44 and 45 are formed on the outer face of the dielectric block 12.

10 The separated electrodes 44 and 45 are formed on the opening end face 12a of the dielectric block 12 so as not to be electrically connected to the outer conductor 17 and the other electrodes 21 to 23. The separated electrode 44 extends from the opening end-  
15 face 12a onto the side face 12e. The separated electrode 45 extends from the opening end-face 12a onto the side face 12d. A part of the respective separated electrodes 44 and 45 extend into the resonance holes 13 and 14. The inner conductors 16 of  
20 the resonance holes 13 and 14, which function as resonance electrodes, are opposed, via the conductor gaps 32, to the separated electrodes 44 and 45 in the resonance holes 13 and 14, in the vicinity of the opening end-face 12a, respectively.

25 Moreover, the PIN diodes D11 and D12 are mounted to both of the side faces 12e and 12d of the

dielectric block 12, respectively. The inductors L11 and L12 are mounted onto the opening end-face 12a.

The PIN diode D11 is electrically connected between the outer conductor and the separated electrode 44.

5 The PIN diode D12 is electrically connected between the outer conductor 17 and the separated electrode 45.

The inductor L11 is electrically connected between the separated electrodes 44 and 45. The inductor L12 is electrically connected between the separated electrode

10 45 and the voltage control terminal electrode 23.

In the dielectric filter 41 having the above-described configuration, the frequency shifting capacitor Cs1 is formed by the separated electrode 44 and the inner conductor 16 of the resonance hole 13 which oppose each other via the conductor gap 32 and generate electrostatic capacitive coupling between the separated electrode 44 and the inner conductor 16 of the resonance hole 13. Similarly, the frequency shifting capacitor Cs2 is formed by the separated electrode 45 and the inner conductor 16 of the resonance hole 14 which oppose each other via the conductor gap 32 to generate electrostatic capacitive coupling between the separated electrode 45 and the inner conductor 16. As a result, the dielectric filter 41 can be reduced in size.

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(Fourth Embodiment, FIG. 7)

As shown in FIG. 7, in a variable frequency dielectric filter 51, the dielectric block 12 is mounted onto a circuit substrate 60 having the PIN diodes D11 and D12 and the inductors L11 and L12  
5 diodes D11 and D12 and the inductors L11 and L12 mounted thereto.

On the upper face of the circuit substrate 60, an input electrode pattern 61, an output electrode pattern 62, and a voltage control electrode pattern  
10 63, relay electrode patterns 65 and 66, and a wide area ground pattern 64 are formed. The PIN diode D11 is electrically connected between the ground pattern 64 and the relay electrode pattern 65. The PIN diode D12 is electrically connected between the ground  
15 pattern 64 and the relay electrode pattern 66. The inductor L11 is electrically connected between the relay electrode patterns 65 and 66. The inductor L12 is electrically connected between the relay electrode pattern 66 and the voltage control electrode pattern  
20 63.

Meanwhile, on the outer face of the dielectric block 12, the outer conductor 17, the input terminal electrode 21, the output terminal electrode 22, and two separated electrodes 54 and 55 are formed. The  
25 separated electrodes 54 and 55 are formed on the under face 12f of the dielectric block 12, respectively, so

as not to be electrically connected to the outer conductor 17 and the input and output terminal electrodes 21 and 22.

The dielectric block 12 is mounted onto the  
5 circuit substrate 60 by use of solder, an electrically  
conductive adhesive, or the like. Thereby, the input  
terminal electrode 21 of the dielectric block 12 is  
electrically connected to the input electrode pattern  
61 of the circuit substrate 60. Similarly, the output  
10 terminal electrode 22 is electrically connected to the  
output electrode pattern 62. The separated electrodes  
54 and 55 are electrically connected to the relay  
electrode patterns 65 and 66, respectively. The outer  
conductor 17 is electrically connected to the ground  
15 pattern 64.

In the dielectric filter 51 having the above-  
described configuration, the frequency shifting  
capacitor Cs1 is formed, due to generation of an  
electrostatic capacitance between the separated  
20 electrode 54 and the inner conductors 16 of the  
resonance holes 13. Similarly, the frequency shifting  
capacitor Cs2 is formed, due to generation of an  
electrostatic capacitance between the separated  
electrode 55 and the inner conductors 16 of the  
25 resonance holes 14. Accordingly, the dielectric  
filter 51 has the same equivalent electric circuit as

that of the electric circuit of FIG. 2 excepting that the coupling adjustment capacitor C11 is excluded. As a result, the small-sized dielectric filter 51 can be obtained.

5        (Fifth Embodiment, FIG. 8)

As shown in FIG. 8, a variable frequency dielectric filter 71 comprises a circuit substrate 80 having the PIN diodes D11 and D12 and the inductors L11 and L12 mounted thereto, bonded to the opening  
10    end-face 12a of the dielectric block 12.

On the front side of the circuit substrate 80, relay electrode patterns 81 and 82, a ground pattern 85, and a voltage control electrode pattern 86 are formed. The relay electrode patterns 81 and 82 are  
15    connected to relay electrode patterns 81a and 82a formed on the back side of the circuit substrate 80, via through-holes 83 provided in the circuit substrate 80. The PIN diode D11 is electrically connected between the ground pattern 85 and the relay electrode  
20    pattern 82. The PIN diode D12 is electrically connected between the ground pattern 85 and the relay electrode pattern 81. The inductor L11 is electrically connected between the relay electrode patterns 81 and 82. The inductor L12 is electrically  
25    connected between the relay electrode pattern 81 and the voltage control electrode pattern 86.



Meanwhile, the outer conductor 17, the input terminal electrode 21, the output terminal electrode 22, two separated electrodes 74 and 75 are formed on the outer surface of the dielectric block 12. The  
5 separated electrodes 74 and 75 are formed on the opening end-face 12a of the dielectric block 12 so as not to be electrically connected to the outer conductor 17, and the input and output terminal electrodes 21 and 22. The inner conductors of the  
10 resonance holes 13 and 14 are opposed, via the conductor gaps 32, to the separated electrodes 74 and 75 elongating in the resonance hole 13 and 14, so as to sandwich the gap 32, in the vicinity of the opening end face 12a.

15 When the circuit substrate 80 is bonded to the opening end face 12a of the dielectric block 12, the relay electrode patterns 81a and 82a of the circuit substrate 80 are electrically connected to the separated electrodes 74 and 75 of the dielectric block  
20 12, respectively.

In the dielectric filter 71 having the above-described configuration, the frequency shifting capacitor Cs1 is formed by the separated electrode 75 and the inner conductor 16 of the resonance hole 13  
25 opposed to each other so as to sandwich the conductor gaps 32 and generate electrostatic capacitive

coupling, respectively. Similarly, the frequency shifting capacitor Cs2 is formed by the separated electrode 74 opposed to the inner conductor 16 of the resonance hole 14 so as to sandwich the conductor gap 32 and generate electrostatic capacitive coupling.

Accordingly, the dielectric filter 71 has substantially the same equivalent circuit as that of the electric circuit shown in FIG. 2 excepting that the coupling adjustment capacitor C11 is excluded. As a result, the dielectric filter 71 can be reduced in size. The height of the filter 71 can be even more reduced as compared with the filter 51 of the fourth embodiment.

(Sixth Embodiment, FIG. 9)

In the dielectric filters described in the first to fifth embodiments, the frequency shifting capacitors are formed by means of the separated electrodes formed on the surfaces of the dielectric blocks, respectively. However, in some cases, with such separated electrodes, electrostatic capacitances can not be satisfactorily produced. Accordingly, in the sixth embodiment, a dielectric filter containing a frequency shifting coupling capacitor having a large electrostatic capacitance is described.

As shown in FIG. 9, a variable frequency dielectric filter 91 comprises the dielectric block

12, the circuit substrate 80 having the PIN diodes D11 and D12 or the like mounted thereon, insulation members 92 and 93 having a desired dielectric constant, and metallic pins 94 and 95 having the same  
5 function as the separated electrodes. The columnar insulation members 92 and 93, while they have the metallic pins 94 and 95 inserted under pressure into the central axial portions thereof, are inserted into the resonance holes 14 and 13, respectively. The  
10 circuit substrate 80 is arranged so as to be opposed to the opening end-face 12a of the dielectric block 12, and the heads of the metallic pins 94 and 95 are inserted through the through-holes 83 of the circuit-substrate 80 and soldered.

15 In the dielectric filter 91 having the above-described configuration, the frequency shifting capacitor Cs1 is formed by generation of an electrostatic capacitance between the metallic pin 95 and the inner conductor 16 of the resonance hole 13.  
20 The frequency shifting capacitor Cs2 is formed by generation of an electrostatic capacitance between the metallic pin 94 and the inner conductor 16 of the resonance hole 14. Thus, the frequency shifting capacitors Cs1 and Cs2 have the structure of a so-  
25 called coaxial capacitor, and therefore, have a large electrostatic capacitance, respectively. The

dielectric capacitor 91 has substantially the same equivalent circuit as that of the electric circuit of FIG. 2 excepting that the coupling adjustment capacitor C11 is excluded.

5           In the dielectric capacitor 91, the input and output terminal electrodes 21 and 22 may be provided on the circuit substrate 80, not on the front surface of the dielectric block 12. Moreover, the electromagnetic shielding may be enhanced by providing  
10   the conductor gaps 32 in the inner conductors 16 of the resonance holes 13 and 14 as shown in FIG. 5, and by covering the opening end face 12a of the dielectric block 12 with the outer conductor 17.

(Seventh Embodiment, FIG. 10)

15           In the seventh embodiment, the frequency shifting capacitors Cs1 and Cs2 are formed of the chip capacitors, if a sufficient electrostatic capacitance can not be obtained by means of the separated electrodes formed on the surface of the dielectric  
20   block. As shown in FIG. 10, a variable frequency dielectric filter 101 comprises the dielectric block 12, the circuit substrate 80 having the PIN diodes D11 and D12 and so forth mounted thereto, and connecting members 102 and 103. The connecting members 102 and  
25   103 are formed by punching a metallic sheet having a spring-like property, and working the metallic sheet

by bending it. The connecting members 102 and 103 are electrically connected to the inner conductors 16 by inserting the feet 104 thereof having a spring-like property into the resonance holes 14 and 13,  
5 respectively. Thus, the members 102 and 103 are secured to the dielectric block 12.

The circuit substrate 80 is arranged so as to be opposed to the opening end-face 12a of the dielectric block 12. The heads of the connecting members 102 and  
10 103 are soldered to the relay electrode patterns 81a and 82a formed on the back side of the circuit substrate 80. On the front side of the circuit substrate 80, the relay electrode patterns 81, 82, 88a, and 88b, the voltage control electrode pattern  
15 86, and the voltage control electrode pattern 86, and the ground patterns 89a and 89b are provided. To the circuit substrate 80, the chip capacitors Cs1 and Cs2 as the frequency shifting capacitors are mounted, in addition to the PIN diodes D11 and D12 and the  
20 inductors L11 and L12.

(Eighth Embodiment, FIG. 11)

The eighth embodiment is substantially the same as the first embodiment excepting that a concavity 112 is provided, instead of the step 18 of the dielectric  
25 filter 11 of the first embodiment. As shown in FIG. 11, in the variable frequency dielectric filter 111,

the concavity 112 is formed on the upper face 12c of the dielectric block 12.

The two separated electrodes 24 and 25, together with a part of the outer conductor 17 and the voltage control terminal electrode 23, are formed in the concavity 112 on the upper face 12c of the dielectric block 12 so as not to be electrically connected to the outer conductor 17 and the other electrodes 21 to 23. In the concavity 112, the PIN diodes D11 and D12, and the inductors L11 and L12 are mounted. The PIN diode D11 is electrically connected between the outer conductor 17 and the separated electrode 24. The PIN diode D12 is electrically connected between the outer conductor 17 and the separated electrode 25. The inductor L11 is electrically connected between the separated electrodes 24 and 25 in parallel to them. The inductor L12 is electrically connected between the separated electrode 25 and the voltage control terminal electrode 23.

In the dielectric filter 111 having the above-described configuration, the frequency shifting capacitors Cs1 and Cs2 are formed by the separated electrodes 24 and 25 formed on the upper face 12c of the dielectric block 12 and the inner conductors 16 of the resonance holes 13 and 14. Furthermore, the PIN diodes D11 and D12 and the inductors L11 and L12 are

mounted in the concavity 112 on the upper face 12c of the dielectric block 12. Accordingly, the dielectric filter 111 can be reduced in size.

(Ninth Embodiment, FIGS. 12 to 14)

5        FIG. 12 is an exploded perspective view showing the ninth embodiment of the dielectric filter of the present invention. FIG. 13 is a cross section taken along line XIII - XIII before the PIN diodes are mounted as shown in FIG. 12. FIG. 14 is a cross  
10      section taken along line XIV - XIV before the PIN diodes are mounted as shown in FIG. 12.

As shown in FIG. 12, the variable frequency band-pass dielectric filter 121 is substantially the same as the dielectric filter 11 of the first embodiment,  
15      excepting that the PIN diodes D11 and D12 are mounted in the resonance holes 13 and 14, respectively. Concretely, the outer conductor 17, the input terminal electrode 21, the output terminal electrode 22, and the separated electrodes 24 and 25 are formed on the  
20      outer face of the single dielectric block 12 having a substantially rectangular parallelepiped shape. A step 18 is formed on the upper face 12c of the dielectric block 12. The inductors L11 and L12 are mounted on the lower portion 19 of the upper face 12c.  
25      Furthermore, the PIN diodes D11 and D12 are formed in the resonance holes 13 and 14. For the purpose of

mounting the PIN diodes D11 and D12, the hole diameters at the opening end-face 12a of the resonance holes 13 and 14 are set to be larger than those at the short-circuited end-face 12b thereof.

5           The separated electrodes 24 and 25 are formed on the lower portion 19 on the upper face 12c of the dielectric block 12 so as not to be electrically connected to the outer conductor 17 and the voltage control terminal electrode 23. As shown in FIG. 13,  
10   the separated electrodes 24 and 25 extend from the upper face 12c to substantially central positions within the resonance holes 13 and 14 via the opening end-face 12a and the inner wall upper-surfaces of the resonance holes 13 and 14, respectively. The  
15   separated electrodes 24 and 25 are extended around the whole of the circumferences of the inner wall surfaces of the resonance holes 13 and 14 substantially in the centers of the resonance holes 13 and 14, respectively (Fig. 13). The inner conductors 16 of the resonance  
20   holes 13 and 14 are opposed at respective gaps 32 to the separated electrodes 24 and 25 in the resonance holes 13 and 14. Furthermore, as shown in FIG. 14, the outer conductor 17 is elongated onto the inner wall lower-surfaces of the resonance holes 13 and 14,  
25   in the vicinity of the opening end-face 12a.

The PIN diode D11 is electrically connected



between the outer conductor 17 and the separated electrode 24 in the resonance hole 13. The PIN diode D12 is electrically connected between the outer conductor 17 in the resonance hole 14 and the  
5 separated electrode 25 in the resonance hole 14. The inductor L11 is electrically connected between the separated electrodes 24 and 25. The inductor L12 is electrically connected between the separated electrode 25 and the voltage control terminal electrode 23.

10 In the dielectric filter 121 having the above-described configuration, the frequency shifting capacitor Cs1 is formed by the separated electrode 24 and the inner conductor 16 of the resonance hole 13 opposed to each other so as to sandwich the conductor  
15 gap 32. Similarly, the frequency shifting capacitor Cs2 is formed by the separated electrode 25 and the inner conductor 16 of the resonance hole 13 opposed to each other so as to sandwich the conductor gap 32. Moreover, the inductors L11 and L12 are mounted onto  
20 the lower portion 19 of the step 18, and moreover, the PIN diodes D11 and D12 are mounted in the resonance holes 13 and 14, respectively. Therefore, the dielectric filter 121 can be reduced in size.

(Tenth Embodiment, FIG. 15)

25 As shown in FIG. 15, the tenth embodiment is the same as the second embodiment, excepting that a

concavity 132 is formed on the opening end-face 12a of the dielectric block 12 of the dielectric filter 31.

The separated electrodes 34 and 35, together with a part of the outer conductor 17, are formed in the  
5 concavity 132 on the opening end-face 12a of the dielectric block 12 so as not to be electrically connected to the outer conductor 17 and the input and output terminal electrodes 21 and 22. The separated electrode 35 is elongated from the opening end-face  
10 12a onto the under face 12f. Respective parts of the separated electrodes 34 and 35 are elongated in the resonance holes 13 and 14. The inner conductors 16 of the resonance holes 13 and 14 are opposed to the separated electrodes 34 and 35 elongating in the  
15 resonance holes 13 and 14 so as to sandwich the conductor gaps 32, in the vicinity of the opening end face 12a, respectively.

Moreover, the PIN diodes D11 and D12, and the coupling adjustment capacitor C11 are mounted in the  
20 concavity 132 on the opening end face 12a of the dielectric block 12. The PIN diode D11 is electrically connected between the outer conductor 17 and the separated electrode 34. The PIN diode D12 is electrically connected between the outer conductor 17  
25 and the separated electrode 35. The coupling adjustment capacitor C11 is electrically connected

between the separated electrodes 34 and 35.

In the dielectric filter 131 having the above-described configuration, the frequency shifting capacitor Cs1 is formed by the separated electrode 34  
5 and the inner conductor 16 of the resonance hole 13 opposed to each other so as to sandwich the conductor gap 32. Moreover, the PIN diodes D11 and D12 and the coupling adjustment capacitor C11 are mounted in the concavity 132 on the opening side end face 12a of the  
10 dielectric block 12. Therefore, the dielectric filter 131 can be reduced in size.

(Eleventh Embodiment, FIG. 16)

The eleventh embodiment describes an embodiment of the antenna sharing device of the present  
15 invention. As shown in FIG. 16, in an antenna sharing device 141, a transmission filter 142 is electrically connected between a transmission terminal Tx and an antenna terminal ANT. A reception filter 143 is electrically connected between a reception terminal Rx  
20 and the antenna terminal ANT. Here, as the transmission filter 142 or the reception filter 143, or both, the filters 11, 31, 41, 51, 71, 91, 101, 111, 121, and 131 of the first to tenth embodiments may be employed. By mounting the filter 11 or the like, the  
25 antenna sharing device 141 of which the design flexibility is large, and the size is reduced can be

realized.

(Twelfth Embodiment, FIG. 17)

The twelfth embodiment describes an embodiment of the communication device of the present invention by way of a portable telephone.

FIG. 17 is an electric circuit block diagram of the RF part of a portable telephone 150. In FIG. 17, an antenna element 152, a duplexer 153, a transmission side isolator 161, a transmission side amplifier 162, a transmission side interstage band-pass filter 163, a reception side amplifier 165, a reception side interstage band pass filter 166, a reception side mixer 167, a voltage control oscillation device (VCO) 168, and a local band-pass filter 169 are shown.

Here, as the duplexer 153, for example, the antenna sharing device 141 of the above-described eleventh embodiment can be employed. Furthermore, as the transmission-side and/or reception-side interstage band-pass filters 163 and 166, and/or the local band-pass filter 169, for example, the dielectric filters 11, 31, 41, 51, 71, 91, 101, 111, 121, and 131 of the first to tenth embodiments, or the like can be employed. By mounting the antenna sharing device 141, the dielectric filter 11, or the like, the design flexibility of the RF part can be enhanced, and a small sized portable telephone can be realized.

(Other Embodiments)

The dielectric filter, the antenna sharing device, and the communication device of the present invention are not limited to the above-described  
5   embodiments, and can be variously modified without departing from the spirit and scope of the invention. As the voltage controllable reactance element, a field effect transistor, a variable capacitance diode, or the like may be employed. Furthermore, the dielectric  
10   block may have at least one resonance hole.

As described above, according to the present invention, predetermined capacitances are generated between the separated electrodes and the resonance electrodes, and are used as capacitance components  
15   equivalent to the frequency shifting capacitors. Accordingly, conventional frequency shifting capacitor elements can be omitted. By electrically connecting the voltage controllable reactance element and the circuit element for controlling the reactance element  
20   to the separated electrodes, the reactance element can be voltage controlled to be switched whereby the frequency shifting coupling capacitors formed by the separated electrodes are grounded or opened to shift the frequency characteristic of the filter.

25       Moreover, by electrically connecting at least two separated electrodes via the coupling adjustment

element, the coupling degree between the resonators obtained when the voltage controllable reactance element is on, and that obtained when the voltage controllable reactance element is off can be

5 independently set by use of a smaller number of parts and less current consumption. As a result, an antenna device and a communication device of which the design flexibilities are large, and the sizes are reduced can be obtained.

10 The dielectric filter in accordance with the present invention may comprise a dielectric block having at least one resonance hole, a conductor inserted into the resonance hole while the conductor is insulated from an inner conductor of the resonance  
15 hole, a voltage-controllable reactance element electrically connected to the conductor, and a circuit substrate for the reactance element to be mounted onto, disposed on an outer face of the dielectric block excluding the under face thereof. Accordingly,  
20 a conventional frequency shifting capacitor doesn't need to be provided, since the inner conductor in the resonance hole and the conductor inserted into the resonance hole form a frequency shifting capacitor.

The dielectric filter in accordance with the  
25 present invention may comprise a dielectric block having at least one resonance hole, a conductor

electrically connected to an inner conductor of the  
resonance hole, a voltage-controllable reactance  
element electrically connected to the conductor, and a  
circuit substrate for the reactance element to be  
5 mounted onto, disposed on an outer face of the  
dielectric block excluding the under face thereof.  
Therefore, on the circuit substrate, a circuit element  
for controlling the frequency shifting capacitor  
element and the reactance element, and so forth can be  
10 mounted. Thus, the filter can be reduced in size.

Preferably, either a step or a concavity may be  
provided on the dielectric block, and the separated  
electrode is provided on the step or in the concavity.  
Since the reactance element and the circuit element  
15 can be mounted on the step or in the concavity. the  
size of the dielectric filter can be reduced.

Although the present invention has been described  
in relation to particular embodiments thereof, many  
other variations and modifications and other uses will  
20 become apparent to those skilled in the art.  
Therefore, the present invention is not limited by the  
specific disclosure herein.